# 6.9 Waves in a rod of circular cross-section

cylindrical coordinates : displacements :

equations of motion

$$\nabla^2 u - \cdots = \frac{1}{c_L^2} \frac{\partial^2 u}{\partial t^2}$$
(6.92)

$$\nabla^2 v - \frac{v}{r^2} + \frac{2}{r^2} \frac{\partial u}{\partial \theta} + \frac{1}{1 - 2\nu} \frac{1}{r} \frac{\partial \Delta}{\partial \theta} = \frac{1}{c_T^2} \frac{\partial^2 v}{\partial t^2}$$
(6.93)

$$\nabla^2 w + \cdots = \frac{1}{c_T^2} \frac{\partial^2 w}{\partial t^2}$$
(6.94)

$$\nabla^{2} = \frac{\partial^{2}}{\partial r^{2}} + \frac{1}{r}\frac{\partial}{\partial r} + \frac{1}{r^{2}}\frac{\partial^{2}}{\partial \theta^{2}} + \frac{\partial^{2}}{\partial z^{2}} \qquad (6.95)$$

$$\triangle = \nabla \cdot (u \mathbf{i}_{\mathrm{r}} + v \mathbf{i}_{\Theta} + w \mathbf{i}_{z}) = \frac{\partial u}{\partial r} + \frac{1}{r} \left( \frac{\partial v}{\partial \theta} + u \right) + \frac{\partial w}{\partial z} :$$
(6.96)

axisymmetric (axially symmetric)  $\rightarrow$  §6.10

# \$2.13 summary of equations in cylindrical coordinates displacement potentials

$$(2.132) u = \frac{\partial \phi}{\partial r} + \frac{1}{r} \frac{\partial \psi_z}{\partial \theta} - \frac{\partial \psi_\theta}{\partial z}$$

$$(2.133) v = \frac{1}{r} \frac{\partial \phi}{\partial \theta} + \frac{\partial \psi_r}{\partial z} - \frac{\partial \psi_z}{\partial r}$$

$$(2.134) w = \frac{\partial \phi}{\partial z} + \frac{1}{r} \frac{\partial (\psi_\theta r)}{\partial r} - \frac{1}{r} \frac{\partial \psi_r}{\partial \theta}$$

equations of motion

(2.135) 
$$\nabla^2 \phi = \frac{1}{c_L^2} \frac{\partial^2 \phi}{\partial t^2}$$
(6.100)

(2.139) 
$$\nabla^2 \psi_z = \frac{1}{c_T^2} \frac{\partial^2 \psi_z}{\partial t^2}$$
 (6.101)

(2.137) 
$$\nabla^2 \psi_r - \frac{\psi_r}{r^2} - \frac{2}{r^2} \frac{\partial \psi_\theta}{\partial \theta} = \frac{1}{c_T^2} \frac{\partial^2 \psi_r}{\partial t^2}$$
(6.102)

(2.138) 
$$\nabla^2 \psi_{\theta} - \frac{\psi_{\theta}}{r^2} + \frac{2}{r^2} \frac{\partial \psi_r}{\partial \theta} = \frac{1}{c_T^2} \frac{\partial^2 \psi_{\theta}}{\partial t^2}$$
(6.103)

boundary conditions

(2.144) 
$$\sigma_r = \lambda \Delta + 2 G \frac{\partial u}{\partial r} =$$
 at  $r = a$  (6.97) (6.104a)

(2.147) 
$$\tau_{r\theta} = G\left[\frac{1}{r}\left(\frac{\partial u}{\partial \theta} - v\right) + \frac{\partial v}{\partial r}\right] =$$
 (6.98) (6.104b)

(2.149) 
$$au_{rz} = G\left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial r}\right) =$$
 (6.99) (6.104c)

at	r = 0,	(solid cross-section)
at	$r = r_i$ ,	(hollow cross-section)

solutions of the form (

# 6.10 Waves in a circular rod of solid cross-section

motions which are independent of  $\theta$  but do depend on z (

- torsional waves
- longitudinal waves

motions which depend on both  $\boldsymbol{z}$  and

- flexural waves

## 6.10.1 torsional waves

circumferential displacement independent of  $\theta \ \, \Rightarrow \ \, v(r,\,z,\,t)$  equation of motion

$$(6.93) \rightarrow \nabla^{2}v - \frac{v}{r^{2}} = \frac{1}{c_{T}^{2}} \frac{\partial^{2}v}{\partial t^{2}}, \qquad \nabla^{2} = \frac{\partial^{2}}{\partial r^{2}} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{\partial^{2}}{\partial z^{2}}$$
$$\Rightarrow \frac{\partial^{2}v}{\partial r^{2}} + \frac{1}{r} \frac{\partial v}{\partial r} - \frac{v}{r^{2}} + \frac{\partial^{2}v}{\partial z^{2}} = \frac{1}{c_{T}^{2}} \frac{\partial^{2}v}{\partial t^{2}} \qquad (6.124)$$

if not circular  $\rightarrow$ 

separation of variables

$$\begin{array}{l} v(r,\,z,\,t) \;=\; \\ R^{\,\prime\prime}\;+\; \frac{1}{r}\,R^{\prime}\;-\; \frac{1}{r^2}\,R\;-\; k^2\,R\;\;=\; -\; \frac{\omega^2}{c_T^{\,2}}\,R \end{array}$$

(i) if 
$$k = \omega/c_T$$
  
 $R'' + \frac{1}{r}R' - \frac{1}{r^2}R = 0$   
 $R(r) = R$  is at  $r = 0 \rightarrow$   
 $v(r, z, t) = A r \exp[i(kz - \omega t)]$  (6.127)  
satisfies  $\tau_{r\theta} = G\left(\frac{\partial v}{\partial r} - \frac{v}{r}\right) =$  at  $r = a$  automatically  
lowest torsional mode  $c = \omega/k =$ 

(ii) if 
$$k \neq \omega/c_T$$

$$r^{2} R'' + r R' + (q^{2} r^{2} - 1) R = 0 \qquad q^{2} = \frac{\omega^{2}}{c_{T}^{2}} - k^{2} \qquad (6.128)$$

$$R(r) = A J_{1}(qr) + B Y_{1}(qr) \qquad R \text{ is finite (or 0) at } r = 0 \rightarrow$$

$$v(r, z, t) = A J_{1}(qr) \exp[i(kz - \omega t)] \qquad (6.125)$$

$$\tau_{r\theta} = G\left(\frac{\partial v}{\partial r} - \frac{v}{r}\right) = 0 \qquad \text{at } r = a$$

$$\frac{d}{dr}[J_{1}(qr)] = q J_{0}(qr) - \frac{1}{r}J_{1}(qr) = -q J_{2}(qr) + \frac{1}{r}J_{1}(qr)$$

$$J_{2}(qa) = 0 \qquad qa = \qquad (6.126)$$

higher torsional modes (

#### 6.10.2 longitudinal waves

displacement components in the radial and axial directions

independent of 
$$\theta \Rightarrow$$
  
 $u = \frac{\partial \phi}{\partial r} - \frac{\partial \psi_{\theta}}{\partial z}$ ,  $w = \frac{\partial \phi}{\partial z} + \frac{1}{r} \frac{\partial (\psi_{\theta} r)}{\partial r} \rightarrow$ 

equations of motion

$$(6.102) \rightarrow \nabla^{2}\phi = \frac{1}{c_{L}^{2}} \frac{\partial^{2}\phi}{\partial t^{2}} \qquad \Rightarrow \qquad \frac{\partial^{2}\phi}{\partial r^{2}} + \frac{1}{r} \frac{\partial\phi}{\partial r} + \frac{\partial^{2}\phi}{\partial z^{2}} = \frac{1}{c_{L}^{2}} \frac{\partial^{2}\phi}{\partial t^{2}}$$

$$(6.103) \rightarrow \nabla^{2}\psi_{\theta} - \frac{\psi_{\theta}}{r^{2}} = \frac{1}{c_{T}^{2}} \frac{\partial^{2}\psi_{\theta}}{\partial t^{2}} \qquad \Rightarrow \qquad \frac{\partial^{2}\psi_{\theta}}{\partial r^{2}} + \frac{1}{r} \frac{\partial\psi_{\theta}}{\partial r} - \frac{\psi_{\theta}}{r^{2}} + \frac{\partial^{2}\psi_{\theta}}{\partial z^{2}} = \frac{1}{c_{T}^{2}} \frac{\partial^{2}\psi_{\theta}}{\partial t^{2}}$$

separation of variables and solutions

$$\begin{split} \phi(r, z, t) &= \Phi(r) \, \exp[i \, (k \, z - \omega \, t)] \\ &= A \, J_0(p \, r) \, \exp[i \, (k \, z - \omega \, t)] \qquad p^2 \, = \, \frac{\omega^2}{c_L^2} - k^2 \\ \psi_\theta(r, z, t) &= \Psi(r) \, \exp[i \, (k \, z - \omega \, t)] \\ &= C \, J_1(q \, r) \, \exp[i \, (k \, z - \omega \, t)] \qquad q^2 \, = \, \frac{\omega^2}{c_T^2} - k^2 \end{split}$$

$$u(r, z, t) =$$
 $w(r, z, t) =$ 
(6.129)
(6.130)

boundary conditions

$$\begin{split} \sigma_r &= \lambda \left( \frac{\partial u}{\partial r} + \frac{u}{r} + \frac{\partial w}{\partial z} \right) + 2 G \frac{\partial u}{\partial r} = & \text{at } r = a \\ &\Rightarrow \left[ -\frac{1}{2} (q^2 - k^2) J_0(pa) + \frac{p}{a} J_1(pa) \right] A + \left[ -i k q J_0(qa) + \frac{ik}{a} J_1(qa) \right] C = & \cdots \text{(1)} \\ \tau_{rz} &= G \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial r} \right) = & \text{at } r = a \\ &\Rightarrow \left[ -2 i k p J_1(pa) \right] A - (q^2 - k^2) J_1(qa) C = & \cdots \text{(2)} \end{split}$$

$$(1), (2) \Rightarrow \text{ nontrivial condition for } A, C 
$$\frac{2p}{a} (q^2 + k^2) J_1(pa) J_1(qa) - (q^2 - k^2)^2 J_0(pa) J_1(qa) - 4k^2 p q J_1(pa) J_0(qa) =$$

$$\text{Pochhammer frequency equation}$$

$$(6.131)$$$$

Fig. 6.13dimensionless frequencies  $(\omega a/\pi c_T)$ vs.dimensionless wavenumber  $(ka/\pi)$ Fig. 6.14dimensionless phase velocity  $(c/c_b)$ vs."" $(ka/2\pi)$ Fig. 6.15dimensionless group velocity  $(c_g/c_b)$ vs."" $(ka/2\pi)$ 

ex.

#### 6.10.3 flexural waves

non-axisymmetric motion ( skip )

## 6.11 Approximate theories for rods

wave motions in rods of arbitrary cross-sections can be described by one-dimensional approximate theories.

ex.

#### 6.11.1 longitudinal motions

assumption : Cross-sectional area of the rod remains

$$\frac{\partial^2 u}{\partial x^2} = \frac{1}{c_b^2} \frac{\partial^2 u}{\partial t^2} \qquad c_b^2 =$$

Axial shear modes and radial modes are

## 6.11.2 torsional motions

assumption : Transverse sections remain

The motion consists of a rotation of the sections about the axis.

(Both the warping and the in-plane motions are neglected)

$$\frac{\partial^2 v}{\partial x^2} = \frac{1}{c^2} \frac{\partial^2 v}{\partial t^2} \qquad c^2 =$$

J: torsional constant (GJ:

I: moment of inertia (J = I for a circular cross-section)

radius of gyration 
$$k \Rightarrow I =$$

$$c^2 = \frac{D}{\rho A k^2} \qquad \Rightarrow \qquad c = \sqrt{\frac{D}{\rho A}} \frac{1}{k}$$
(6.142)

## 6.11.3 flexural motions

assumption :

1. Dominant displacement component is parallel to the plane of symmetry.

2. Deflections are small and cross-sectional areas remain plane and normal to the neutral axis.

$$\frac{\partial^2 w}{\partial t^2} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} = 0 \tag{6.143}$$

A : cross-sectional area

I: second moment of the cross-sectional area about the neutral axis

$$w(x,t) = B \exp[ik(x-ct)] \Rightarrow -k^2c^2 + k^4\frac{EI}{\rho A} = 0 \Rightarrow c^2 =$$
  
$$\Rightarrow \qquad c = \sqrt{\frac{E}{\rho}} \sqrt{\frac{I}{A}} k \qquad (6.144)$$
  
$$c \propto k \quad \text{(phase velocity is proportional to the wavenumber)}$$

correct for small wavenumbers (long waves)

for a circular cylindrical rod  $(I = \Rightarrow \frac{I}{A} = \frac{1}{4})$  $c = \frac{1}{2}\sqrt{\frac{E}{\rho}}k$ (6.145)

# 6.12 Approximate theories for plates

- 6.12.1 flexural motions classical theory
- 6.12.2 effects of transverse shear and rotary inertia
- 6.12.3 extensional motions

## ( skip )